THE MIXING AND SEGREGATION EFFECTS DURING SHEAR DEFORMATION OF COHESIONLESS PARTICULATE SOLIDS

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Abstract: The mixing and segregation kinetics in the course of shear flow of particulate solids at low shear rates is studied analytically and experimentally. Only one experimental constant (segregation coefficient) is used to forecast the segregation and mixing dynamics of nonelastic cohesionless rough spherical particles.

Introduction

In our previous paper [1] we have suggested the experimental unit and method of segregation and mixing exploration during shear deformation of participate solids. Then a mathematical description of the mixing effect during shear flow of participate solids was carried out. The kinetic parameters of the mixing flux were determined on the basis of the analysis of chaotic transversal movements of spherical nonelastic cohesionless particles (transversal mass transfer) in a restricted environment. These chaotic movements are formally analogous to the quasi-diffusional mixing of particles.

That is why the mixing flux of particles is expressed as the quasi-diffusional mixing flux in the transversal direction

\[ j_m = -D_{\text{dif}} \rho_b (\partial c/\partial y) = -0.5 \rho_b u_t (\partial \bar{c}/\partial y) , \]  

where \( D_{\text{dif}} \) is the coefficient of quasi-diffusional mixing; \( c \) is the concentration of test particles; \( s \) is the mean; distance between particles \( \rho_b \) is the bulk density of particulate solids. The mean relative transversal velocity between particles of neighbouring flow layers is calculated on the basis of the analysis of chaotic transversal movements of spherical nonelastic cohesionless particles (transversal mass transfer) in a restricted environment (Fig. 1)

\[ u_t = (du/\partial y)bd \sin((\pi/4)(d + s)/d) , \]

where \( d \) is the mean particle diameter; \( b = (\pi/(6(1 - \varepsilon)))^{0.33} \) is the geometrical parameter; \( b_0 \) is the geometrical parameter \( b \), calculated at \( \varepsilon = \varepsilon_0 = 0.2595 \), \( \varepsilon \) is the fraction of void volume.
However, the real particulate solids is not uniform in complex of physical and mechanical properties and then the chaotic movements are accompanied by systematic displacements of particles because of segregation effects.

Although segregation has long been known and has been used over centuries in human activities, e.g. in grain and cereal cleaning, gold dust mining, etc., the scientific cognition of this physical phenomenon is still in its infancy [2]. This is because the segregation phenomenon, albeit simple in appearance, has extremely complex and diverse physical mechanisms.

In the context of the above, it is very important to perform investigations to reveal mechanisms and kinetic laws of segregation for the most general and practically important cases of flow of granular media, e.g., shear deformation flows.

The segregation flux $j_s$ is determined on the basis of the mechanism of hydromechanical segregation [3], which developed here in terms of «slow» shear flow of particulate solids when prolonged interparticle contacts take place.

Taking into account the fact that the segregation kinetics at low shear rates doesn't depend practically on the shear stress we formulated the segregation driving force as the relative excess moment of forces acting on a test particle in a nonuniform medium

$$\Delta M_t = (M - M_0)/M_0,$$  \hspace{1cm} (3)

where $M = M_g + M_f$ is the sum moment of gravity $M_g$, friction $M_f$ forces acting on a test particle of the mixture, $M_0$ is analogous moment acting on an average particle of the mixture. These moments are calculated analytically.

Taking into account that the segregation intensity is proportional to the shear rate [4] we expressed the segregation flux in the following way

$$j_s = K_s \rho b u_r \Delta M_t = K_s \rho b (du/\lambda y)\Delta M_t,$$  \hspace{1cm} (4)

where $K_s$ is the segregation coefficient, $u_r$ is the mean relative shear velocity between interacting particles.

Method of segregation coefficient determination in according with (4) the segregation coefficient acquires the physical sense of the relation between transversal and tangent velocities of test particles and $\Delta M_t$ parameter is adequate to the separation factor which determines the inclination of mixture particles to segregation.
Then the segregation coefficient is determined as follows

\[ K = \frac{u_t}{(\Delta M_c b d)(du/\,dy)} \]  

(5)

where \( u_t \) is the mean transversal velocity of a single test particle determined experimentally in the conveyor shear cell [1] using uniform bulk particles.

The experimental results of a segregation coefficient investigation are shown on Figs. 2 and 3.

**Fig. 2. Segregation coefficient dependence on the test particle diameter \((a)\) and the shear rate \((b)\) for glass beads \((d_b = 3.5 \times 10^{-3} \text{ m})\)**

**Fig. 3. Segregation coefficient dependence on the test particle diameter \((a)\) and the shear rate \((b)\) for ceramic granules \((d_b = 6.6 \times 10^{-3} \text{ m})\)**
Mathematical simulations of segregation and mixing effects

The mathematical description of the joint segregation and mixing effect in the course of shear deformation of particulate solids is based on the general mass transfer equation, which was adapted here to the steady two-dimensional shear flow as follows

\[ \frac{\partial \rho_p}{\partial t} = \frac{\partial}{\partial x} \left( u \frac{\partial \rho_p}{\partial x} \right) + \frac{\partial}{\partial y} \left( j_{m} - j_{y} \right) / \partial y, \]  

(6)

where \( u \) is the mean particle velocity towards shear direction \( x \), \( (x, y) \). Cartesian coordinates, \( \tau \) is the time.

The boundary conditions for Eq. (6) are formulated in the absence of transverse material flows at the upper and lower boundaries

\[ \frac{\partial (j_{m})}{\partial y} = \frac{\partial (j_{y})}{\partial y} = 0, \quad \text{when} \quad y = 0, h, \]  

(7)

where \( h \) is the bed height. The initial condition has the form

\[ \begin{cases} c(0 < x \leq 0.04, y, 0) = 1; \\ c(x > 0.04, y, 0) = 0. \end{cases} \]  

(8)

The kinetic parameters \( D_{\text{dif}}, \) and \( \Delta M_{r} \) of this equation are calculated by means of Eqs. (1)–(3). The kinetic constant \( K_{k} \) is found experimentally (Figs. 2 and 3). The flow characteristics, such as \( u(y) \) and \( \varepsilon(y) \), were gotten experimentally by means of the method using the conveyor shear cell [1], e.g. see Fig. 4.

Eq. (6) is integrated numerically. The comparison of the calculated and experimental results shown on Figs. 5 and 6 reveals their adequacy. The standard deviation between the named results of segregation and mixing dynamics modeling is 5…6 percentage.

Fig. 4. Velocity (a) and the fraction of void volume (b) profiles during shear deformation of ceramic granules (1) and glass beads (2) in the conveyor shear cell
Fig. 5. Segregation dynamics during shear deformation of ceramic granules ($d_t = 4.4 \cdot 10^{-3}$ m, $d_b = 6.6 \cdot 10^{-3}$ m) in the conveyor shear cell at the mean shear rate 0.475 s$^{-1}$:
1 – experimental; 2 – calculated

Fig. 6. Segregation dynamics during shear deformation of glass beads ($d_t = 3.1 \cdot 10^{-3}$ m, $d_b = 3.5 \cdot 10^{-3}$ m) in the conveyor shear cell at the mean shear rate 0.76 s$^{-1}$:
1 – experimental; 2 – calculated
Conclusions

The suggested mathematical simulation has rather high predictive power, which is confirmed by the results of studying the segregation kinetics and dynamics. Furthermore, the study showed that not only can the mathematical model of the shear flow separation mechanism be used to describe the separation of a mixture of particles, but also this model can be applied to predict the velocities of both small and large single spherical cohesionless particles during shear deformation using a single kinetic coefficient.

References

Les effets du mélangeage et de la ségrégation durant la déformation de cohésion des matières en grains non liées

Résumé: Est réalisée une étude analytique et expérimentale de la cinétique de la ségrégation et du mélangeage durant l’écoulement de cohésion des matières avec des basses vitesses de la cohésion. La prévision de la dynamique de la ségrégation et du mélangeage des particules inélastiques non liées est réalisée avec l’utilisation d’une seule constante expérimentale – coefficient de la ségrégation.

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